



# Trustworthiness in Robust Hypersonic Trajectory Planning

Edmond Jonckheere and Paul Bogdan

Dept. of Electrical and Computer Engineering

University of Southern California, Los Angeles, CA 90089, USA

{jonckhee,pbogdan}@usc.edu

Joseph Winkin

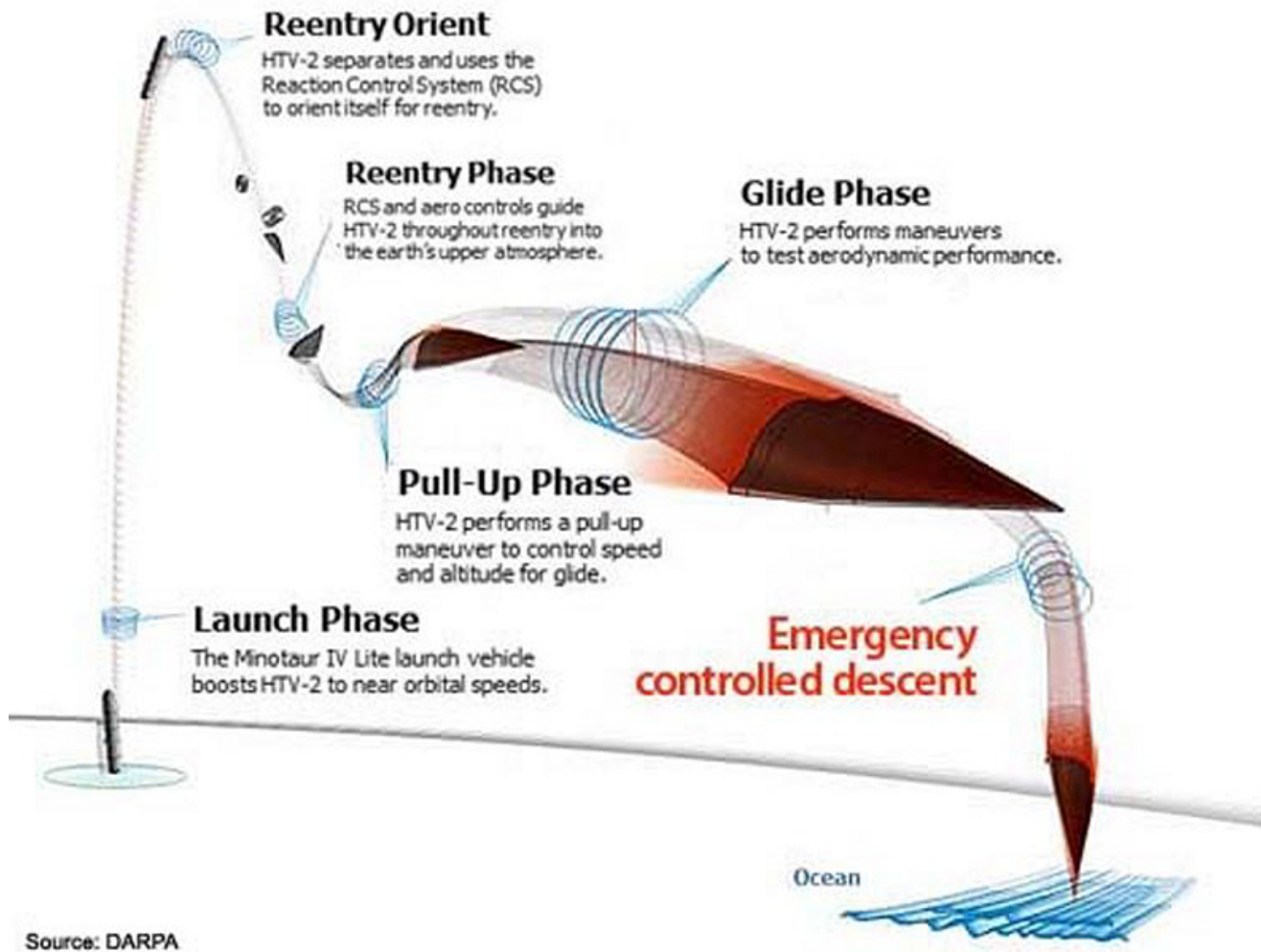
Unité de recherche en mathématiques appliquées et complexité

Université de Namur, B-5000 Namur, Belgique

joseph.winkin@unamur.be

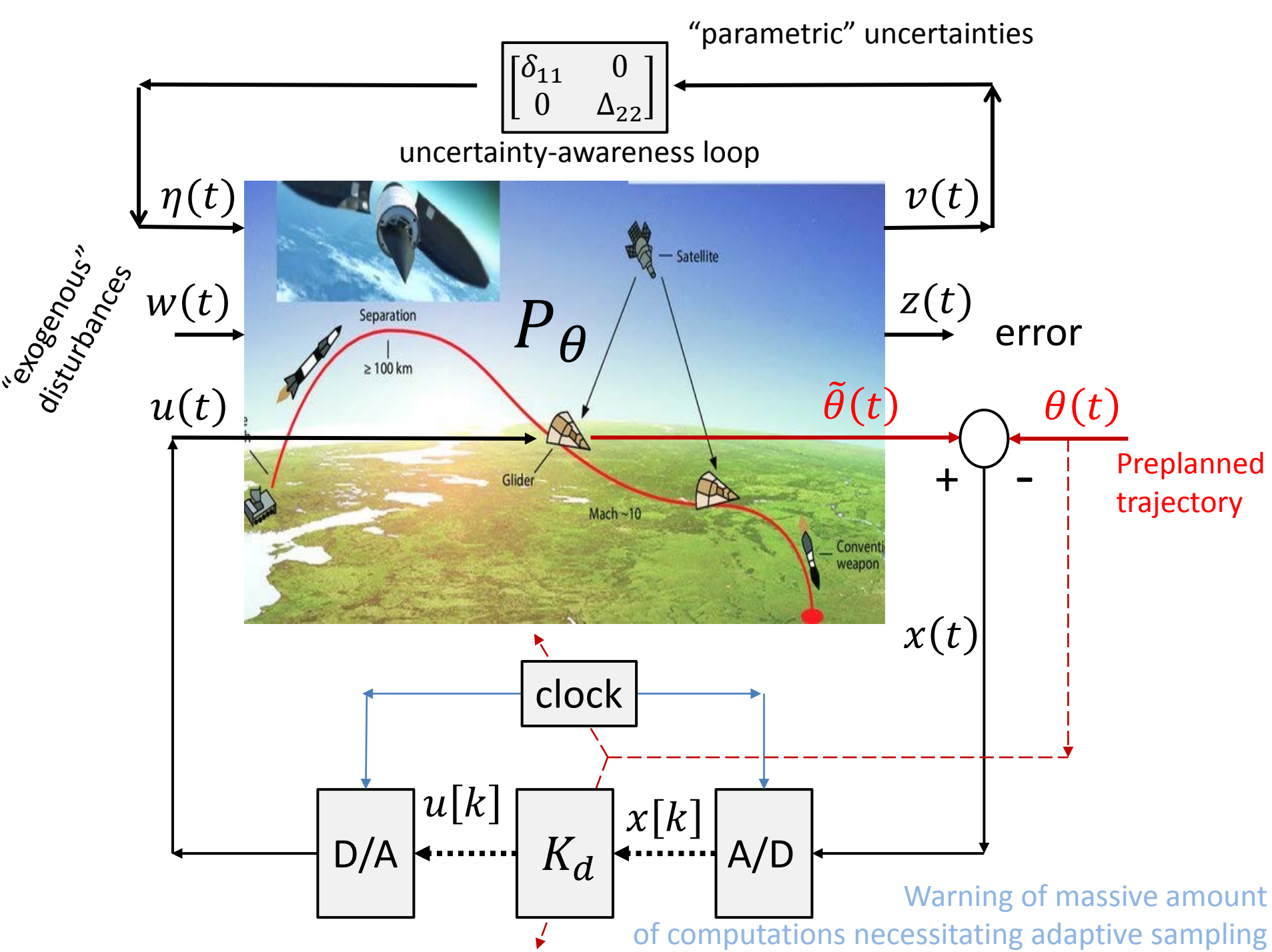


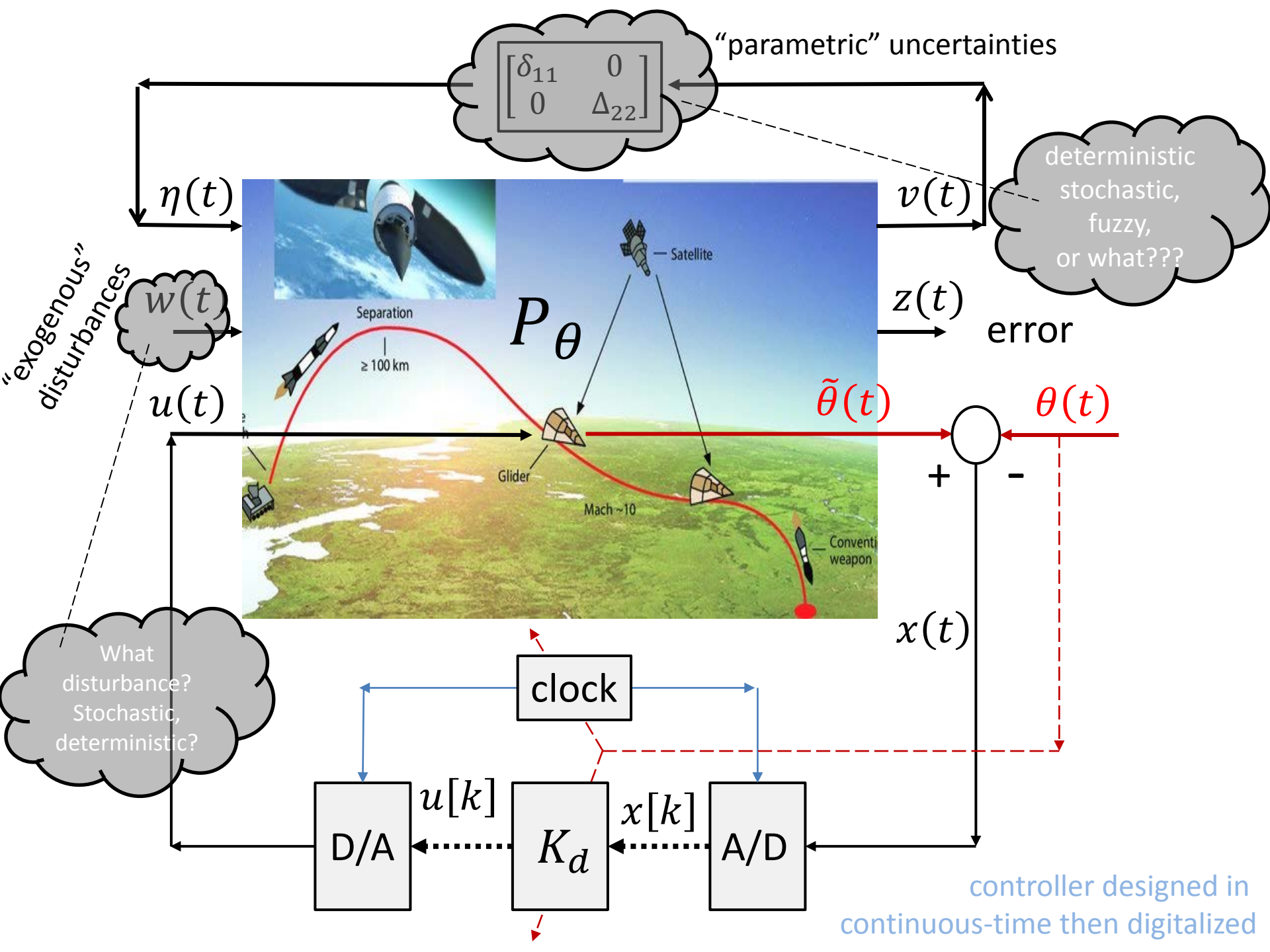
“This solicitation is seeking advancement **to build trust...** and metrics and to quantify uncertainty versus performance... Proposed solutions should.. focus.. on **ways to build trust and confidence** in mission planning. New **methods to improve robustness** and confidence... will still be able to expand trust/explainability of automated mission planning.”



# Classical Robust Control

- Classical robust control (LQG,  $H^\infty$ ) has been extremely successful at designing *uncertainty-aware* control laws
  - when the uncertainties are modeled deterministically.
- The *robust performance theorem* guarantees “hard” error bounds
  - when the uncertainties are subject to “hard” bounds.





# Critique

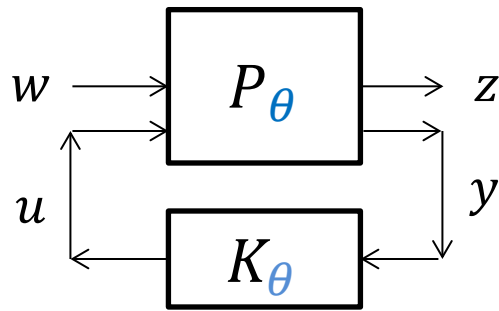
- The “*Achilles heel*” of classical robust control is the modeling of the uncertainty.
- If the modeling of the uncertainty cannot be trusted, the robust control edifice is crumbling.
- Need for trustworthiness assessment
- Quantum control gave us a “heads up.”

I. Khalid, C. A. Weidner, E. Jonckheere, S. G. Schirmer, and F. Langbein, [“Statistically characterizing robustness and fidelity of quantum controls and quantum control algorithms,”](#) *Physical Review A*, vol. 107, page 032606 (22 pages), March 2023.

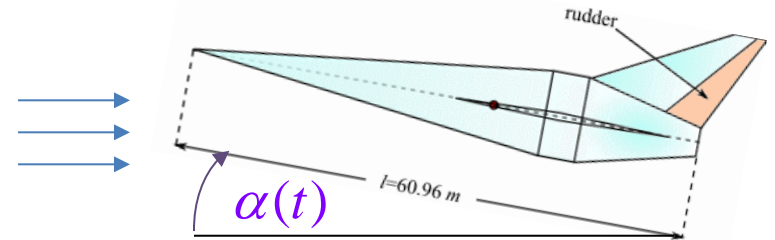
II. S. P. O’Neil, I. Khalid, A. A. Rompokos, C. A. Weidner, F. C. Langbein, S. Shermer, and E. A. Jonckheere, [“Analyzing and unifying robustness measures for excitation transfer control in spin networks,”](#) *IEEE Control Systems Society Letters*, vol. 7, pp. 1783-1788, 2023

# Linear Dynamically Varying *Uncertainty-Unaware* Approach

$$P_\theta: \frac{dx(t)}{dt} = A_{\theta(t)}x(t) + B_{\theta(t)}u(t) + F_{\theta(t)}w(t)$$



$$\left\{ \begin{array}{l} \frac{dx(t)}{dt} = A_{\theta(t)}x(t) + B_{\theta(t)}K_{\theta(t)}y(t) + F_{\theta(t)}w(t) + G_{\theta(t)}\eta(t) \\ x(t) = \tilde{\theta}(t) - \theta(t) \\ y(t) = C_{\theta(t)}x(t) \\ z(t) = \begin{pmatrix} x(t) \\ \delta\alpha(t) \end{pmatrix} \\ u(t) = K_{\theta(t)}y(t) \end{array} \right.$$



$$L^1: \min_u \max_w \frac{\max_\tau \|z(\tau)\|}{\max_\tau \|w(\tau)\|}$$

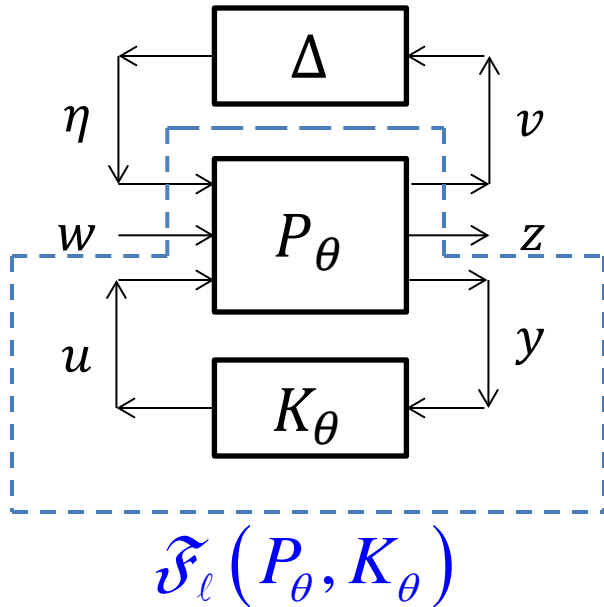
$$H^\infty: \min_u \underbrace{\left( \max_w \frac{\int_t^{t_f} \|z(\tau)\|^2 d\tau}{\int_t^{t_f} \|w(\tau)\|^2 d\tau} \right)^{1/2}}_{\|T_{z \leftarrow w}\|}$$

S. Bohacek and E. A. Jonckheere, "Nonlinear tracking over compact sets with Linear Dynamically Varying  $H^\infty$  control," *SIAM J. Control and Optimization*, vol. 40, No. 4, pp. 1042-1071, 2001.

E. A. Jonckheere, P. Lohsoonthorn, S. Dalzell, "Eigen-structure versus  $H^\infty$  constrained design for hypersonic winged cone," *Journal of Guidance, Dynamics and Control*, AIAA, Vol. 24, No., 4, pp. 648-658, July-August 2001.

# Linear Dynamically Varying *Uncertainty-Aware* Approach

$$P_\theta: \frac{dx(t)}{dt} = A_{\theta(t)}x(t) + B_{\theta(t)}u(t) + F_{\theta(t)}w(t)$$



$$\left\{ \begin{array}{l} \frac{dx(t)}{dt} = A_{\theta(t)}x(t) + B_{\theta(t)}K_{\theta(t)}y(t) + F_{\theta(t)}w(t) + G_{\theta(t)}\eta(t) \\ x(t) = \tilde{\theta}(t) - \theta(t) \\ y(t) = C_{\theta(t)}x(t) \\ z(t) = \begin{pmatrix} x(t) \\ \delta\alpha(t) \end{pmatrix} \\ u(t) = K_{\theta(t)}y(t) \\ v(t) = D_{\theta(t)}x(t) \\ \eta(t) = \Delta v(t) \end{array} \right.$$



Robust performance theorem:

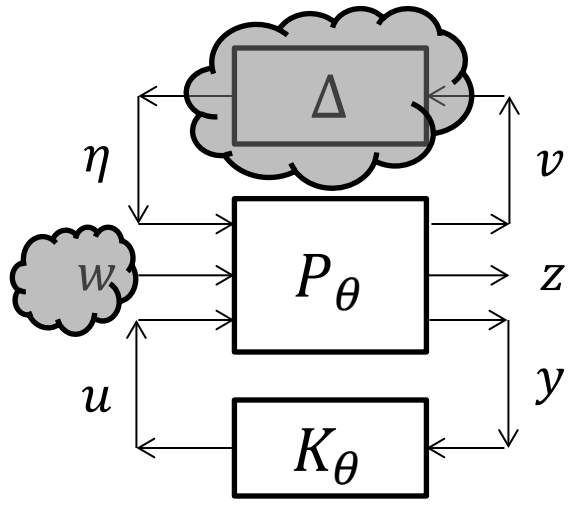
$$\min_{K_{\theta(t)}} \mu\left(\mathcal{F}_l(P_\theta, K_\theta)\right) \Rightarrow \left\|T_{z \leftarrow w}(\Delta)\right\| \leq \mu, \quad \forall \|\Delta\| < 1/\mu$$



# Linear Dynamically Varying *Trust-Aware* Approach

$$P_\theta: \frac{dx(t)}{dt} = A_{\theta(t)}x(t) + B_{\theta(t)}u(t) + F_{\theta(t)}w(t)$$

$$\left\{ \begin{array}{l} \frac{dx(t)}{dt} = A_{\theta(t)}x(t) + B_{\theta(t)}K_{\theta(t)}y(t) + F_{\theta(t)}w(t) + G_{\theta(t)}\eta(t) \\ x(t) = \tilde{\theta}(t) - \theta(t) \\ y(t) = C_{\theta(t)}x(t) \\ z(t) = \begin{pmatrix} x(t) \\ \delta\alpha(t) \end{pmatrix} \\ u(t) = K_{\theta(t)}y(t) \\ v(t) = D_{\theta(t)}x(t) \\ \tilde{\eta}(t) = \Delta v(t) \end{array} \right.$$



Robust performance theorem:

$$\min_{K_{\theta(t)}} \mu(\tilde{\mathcal{F}}_\ell(P_\theta, K_\theta)) \Rightarrow \|T_{z \leftarrow w}(\Delta)\| \leq \mu, \quad \forall \|\Delta\| < 1/\mu$$

How sure are we about this if we are not sure of the uncertainty model?

# Subjective Logic

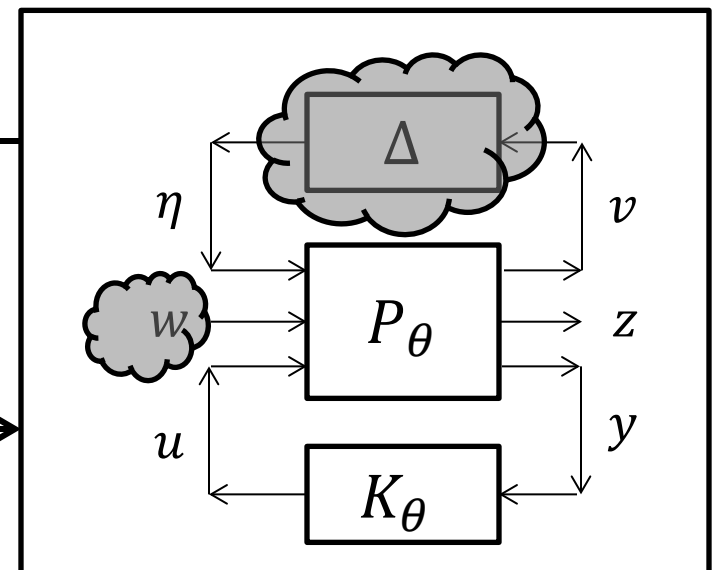
uncertain probability = subjective opinion

- We need an analyst or auditor to assess trustworthiness of the design.

Auditor or Analyst, or trustor, A



Designer, or trustee, x



# Formal Trust Framework

- ❑ **Positive** evidence  $r_x^A$ : Trustor A find that trustee  $x$ 's behavior meets some specifications.
- ❑ **Negative** evidence  $s_x^A$ : Trustor A find that trustee  $x$ 's behavior does not satisfy specifications.
- ❑ **Non-informative** prior weight  $W$  default value  $W=2$
- ❑ **Belief**  $b_x^A = \frac{r_x^A}{r_x^A + s_x^A + W}$
- ❑ **Disbelief**  $d_x^A = \frac{s_x^A}{r_x^A + s_x^A + W}$
- ❑ **Uncertainty**  $u_x^A = \frac{W}{r_x^A + s_x^A + W}$
- ❑ **Base rate**  $a_x^A$ 
  - ❑ Prior probability without evidence default value  $a_x^A = 0.5$

**Opinion:**  $W_x^A = (b_x^A, d_x^A, u_x^A, a_x^A)$

**Trustworthiness:**  $T_x^A = b_x^A + u_x^A a_x^A$

**Risk:**  $R_x^A = d_x^A + u_x^A (1 - a_x^A)$

# Algebra of Opinions

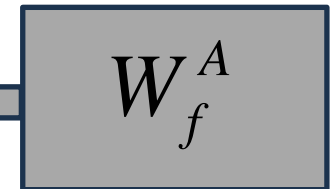
- *Multiplication* of opinions by the same auditor on different sub-designs  $x, y$ :

$$W_{x \cdot y} = W_x \cdot W_y : \begin{cases} b_{x \wedge y} = b_x b_y + \frac{a_y (1 - a_x) b_x u_y + a_x (1 - a_y) b_y u_x}{1 - a_x a_y} \\ d_{x \wedge y} = d_x + d_y - d_x d_y \\ u_{x \wedge y} = u_x u_y + \frac{(1 - a_x) b_y u_x + (1 - a_y) b_x u_y}{1 - a_x a_y} \\ a_{x \wedge y} = a_x a_y \end{cases}$$

Opinion on state feedback  
given filter



Opinion on filter



$$W_K^A = W_{K|f}^A \cdot W_f^A$$

# Algebra of Opinions

- *Fusion* of opinions of two auditors on the same design  $x$ ,

$$W_x^{A \circ B} = W_x^A \circ W_x^B : \begin{cases} b_x^{A \circ B} = \frac{b_x^A u_x^B + b_x^B u_x^A}{u_x^A + u_x^B} \\ u_x^{A \circ B} = \frac{2u_x^A u_x^B}{u_x^A + u_x^B} \\ a_x^{A \circ B} = \frac{a_x^A + a_x^B}{u_x^A + u_x^B} \end{cases}$$

# Trustworthiness of Shapiro (Lockheed) eigenvector assignment

**0,1** X

$$r_v^A = 4, s_v^A = 3$$

$$r_\alpha^A = 3, s_\alpha^A = 4$$

$$r_q^A = 1, s_q^A = 6$$

$$r_g^A = 1, s_g^A = 6$$

$$r_h^A = 1, s_h^A = 6$$

**Table 2** Desired eigenvectors

Parameter	$V_p$		$V_s$		$V_a$	$V_e$	$V_f$
Eigenvector	$v_1$	$v_2$	$v_3$	$v_4$	$v_5$	$v_6$	$v_7$
Velocity	$x^a$	1 <sup>b</sup>	0 <sup>c</sup>	0	0	$x$	$x$
Angle of attack	0	0	$x$	1	$x$	$x$	$x$
Pitch rate	$x$	$x$	1	$x$	$x$	$x$	$x$
Pitch attitude	1	$x$	$x$	$x$	$x$	$x$	$x$
Altitude	$x$	$x$	$x$	$x$	1	$x$	$x$
Symmetric elevon	$x$	$x$	$x$	$x$	$x$	1	0
Fuel equivalent ratio	$x$	$x$	$x$	$x$	$x$	0	1

<sup>a</sup>Here  $x$  is an unspecified component.

<sup>b</sup>Here 1 means that some coupling should be present.

<sup>c</sup>Here 0 means that there should be no coupling.

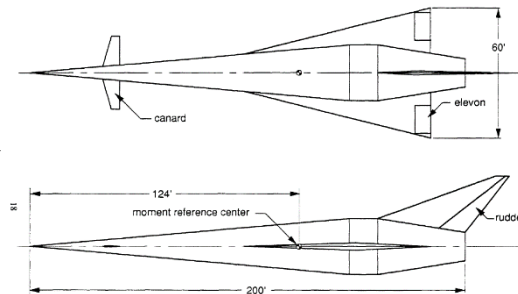
$$T_v^A = \frac{5}{9}, R_v^A = \frac{4}{9}$$

$$T_\alpha^A = \frac{4}{9}, R_\alpha^A = \frac{5}{9}$$

$$T_q^A = \frac{2}{9}, R_q^A = \frac{7}{9}$$

$$T_g^A = \frac{2}{9}, R_g^A = \frac{7}{9}$$

$$T_h^A = \frac{2}{9}, R_h^A = \frac{7}{9}$$



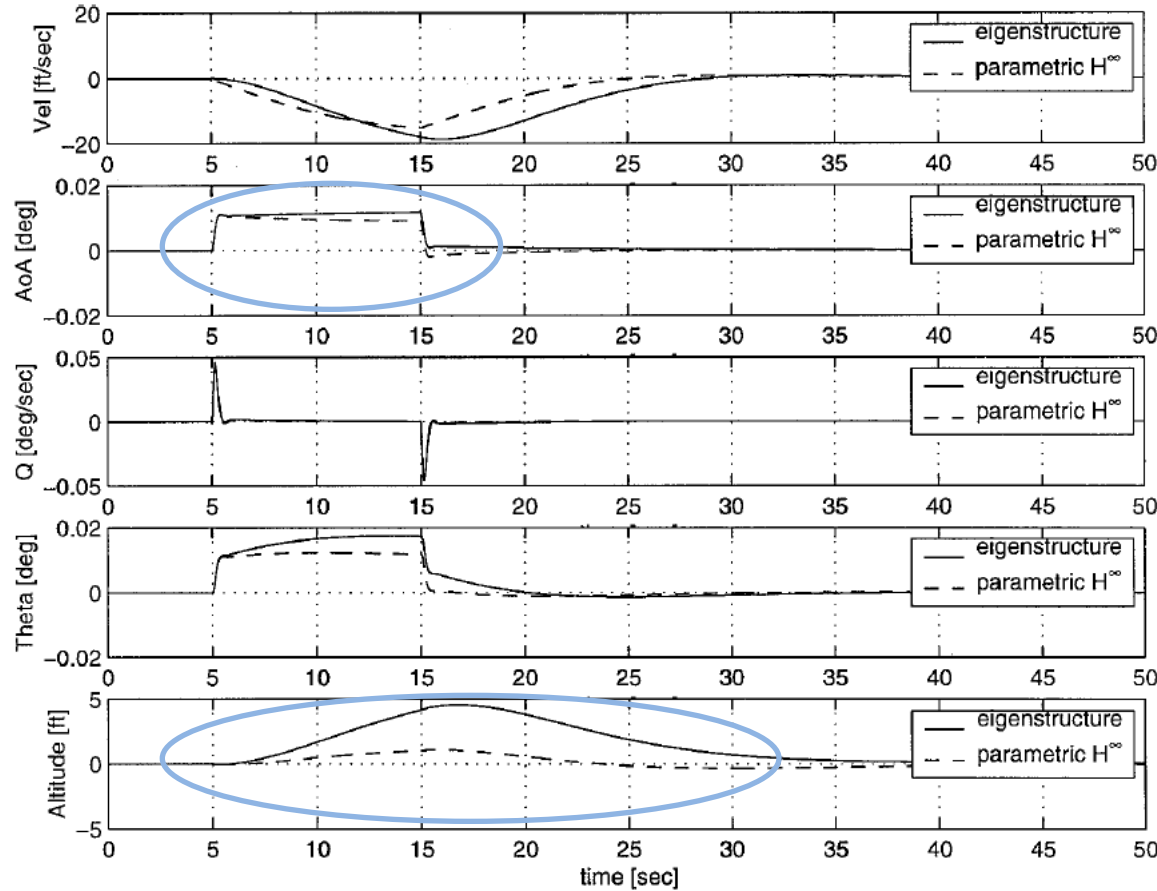
E. Y. Shapiro and J. C. Chung, "[Flight control system synthesis using eigenstructure assignment.](#) *J Optim. Theory Appl.*, Vol. 43, pp. 415–429, 1984.

E. A. Jonckheere, P. Lohsoonthorn, S. Dalzell, "[Eigen-structure versus  \$H^\infty\$  constrained design for hypersonic winged cone,](#)" *Journal of Guidance, Dynamics and Control*, AIAA, Vol. 24, No., 4, pp. 648-658, July-August 2001.

# Trustworthiness and Risk consistent with simulation results

$$T_{\alpha}^A = \frac{4}{9}$$

$$T_h^A = \frac{2}{9}$$



$$R_{\alpha}^A = \frac{5}{9}$$

$$R_h^A = \frac{7}{9}$$

Fig. 8 Velocity, angle-of-attack, pitch-rate, pitch-angle, and altitude time-domain responses to elevon command.

Trustworthiness higher on angle of attack than altitude  
 Risk higher on altitude than angle of attack

# *Off-line* trustworthy trajectory planning

## Uncertainty-aware planning

- Minimize the *error*, which includes the targeting error

$$\min_{\Theta} \left( \min_{K_{\theta}} \mu \left( \mathcal{F}_{\ell} (P_{\theta}, K_{\theta}) \right) \right)$$

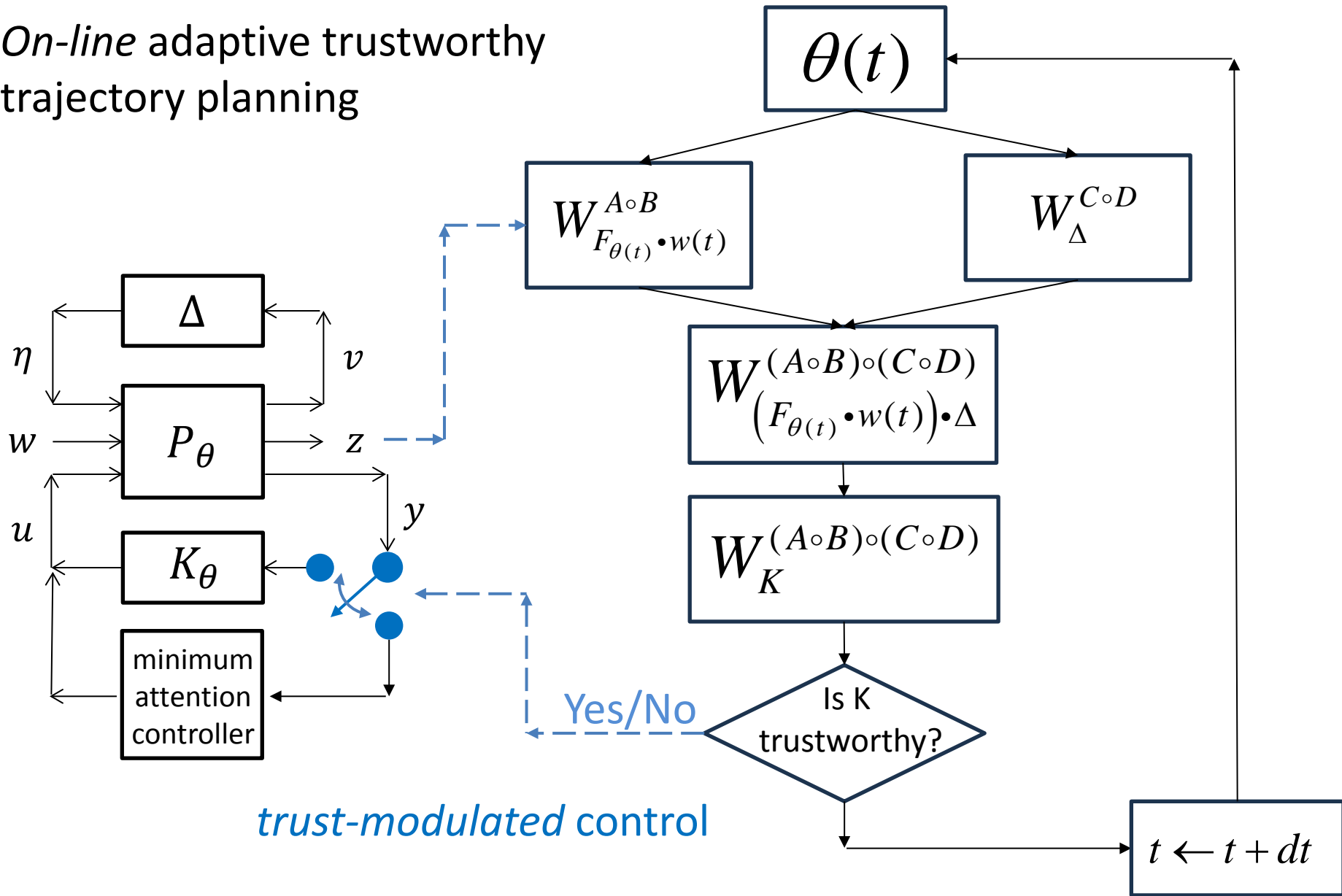
## Trust-aware planning

- Minimize the *risk* of missing the target

$$\min_{\Theta} R_{K_{\theta}}^{(A \circ B) \circ (C \circ D)}$$



# On-line adaptive trustworthy trajectory planning



*trust-modulated control*

J. Shi and D. W. Appley, "A suboptimal N-Step-Ahead cautious controller for adaptive control applications," *J. Dynamic Systems, Measurements and Control*, vol. 120, pp. 419-423, Sept. 1998.

R. W. Brockett, "Minimum attention control," *Proceedings of the 36<sup>th</sup> IEEE Conference on Decision and Control*, San Diego, CA, December 1997, pp. 2628, 1997.

# Conclusions

- Hypersonic mission planning must take into consideration poorly known uncertainties.
- Classical robust control has failed to address trustworthiness of the modeling of the uncertainties.
- We proposed both *off-line* and *on-line* trustworthiness assessments of hypersonic glide vehicles trajectory planning based on subjective logic.
- Early results on a NASA demonstration vehicle showed the viability of the approach.

# Thank you!

## Questions?

[jonckheere@usc.edu](mailto:jonckheere@usc.edu)

[pbogdan@usc.edu](mailto:pbogdan@usc.edu)